

(流動化)

1.

가

()

(Fixed Bed)

(Expanded State)

가

가 “ ”

[1]

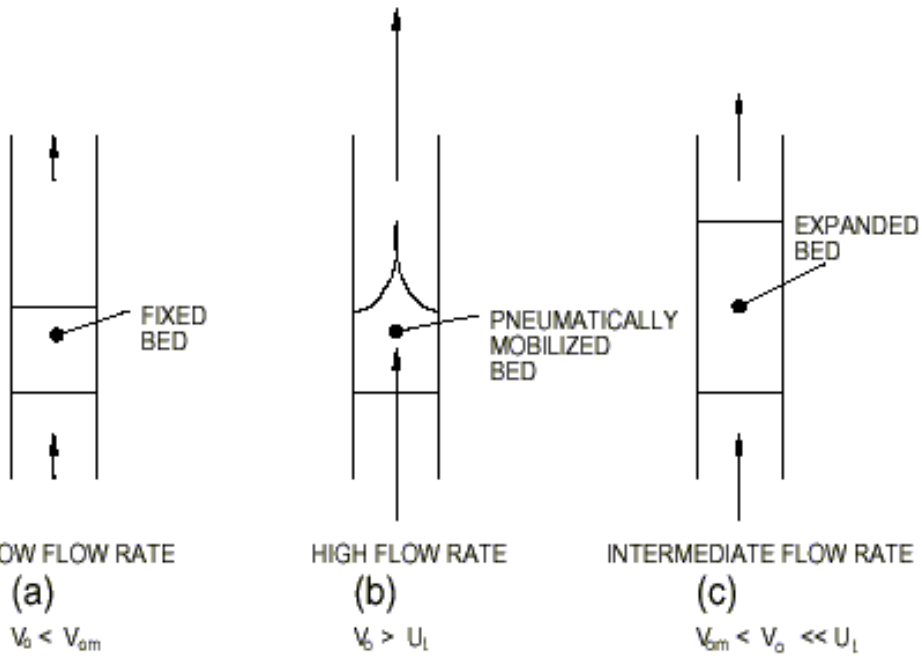
,

V_{om}

가

V_o (

,



[1 : , ,]

(a)

V_o 가

가

V_{om}

U_t

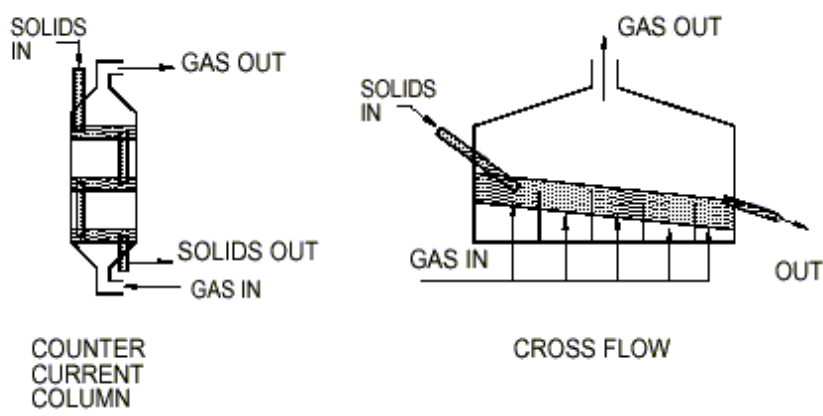
가

가
 V_{om} V_o U_t $V_o < V_{om}$
 V_o U_t
 V_{om} 가
가
가
가 , 가
“ , “
(Fluidization Engineering, 2ed. 1991)

가

- 가 (,)
-
-
- $r_o g h$ (靜壓水頭) 가
- 가

[2 :]



가 - 가 . [

2]

2.

-
-
- /
-
-
- (平床)

가 .

- 가 .
- , .
-
-
- 가 .
- 가 .
-

가 .

-
-
- 가 .
-

3.

●
-
-
-
- (calcinations : 煨燒)

●
●
● ()
●
●
●
●
●
●

4.

“ - “ “ 對 ” (流體相)
4

A :

●
●
-
- 가
- 10 cm
-
●

B : 가

● A 가
● 가 가 V_{om}
● 가

- 가
-

C :

-
- 가 (channel)
-

D :

- 가
-
-
-
-
- 가
-

u^* 對 d_p^*

$$d_p^* = d_p \left[\frac{\mathbf{r}(\mathbf{r}_p - \mathbf{r})}{m^2} \right]^{1/3} = \left(\frac{3}{4} C_D R_{ep}^2 \right)^{1/3} \quad (1)$$

$$u^* = u \left[\frac{\mathbf{r}^2}{m(\mathbf{r}_p - \mathbf{r})g} \right]^{1/3} = \left(\frac{4}{3} \frac{R_{ep}}{C_D} \right)^{1/3} \quad (2)$$

가

-
- u^t
- u_{mf}
- (, , ,)

5.

가 . 가

Ergun

Ergun

가

$$\Delta PA = (\mathbf{r}_p - \mathbf{r})(1 - \mathbf{e}_f)(AL_f) \frac{g}{g_f} \quad (3)$$

(3)

(量)

f

가

$$M_{solids} = \mathbf{r}_p (1 - \mathbf{e}_f) AL_f = constant \quad (4)$$

$$\mathbf{e} \quad L \quad (4)$$

1 2

$$(1 - \mathbf{e}_1)L_1 = (1 - \mathbf{e}_2)L_2 \quad (5)$$

가

(流體相密度)

(3)

對

[3]

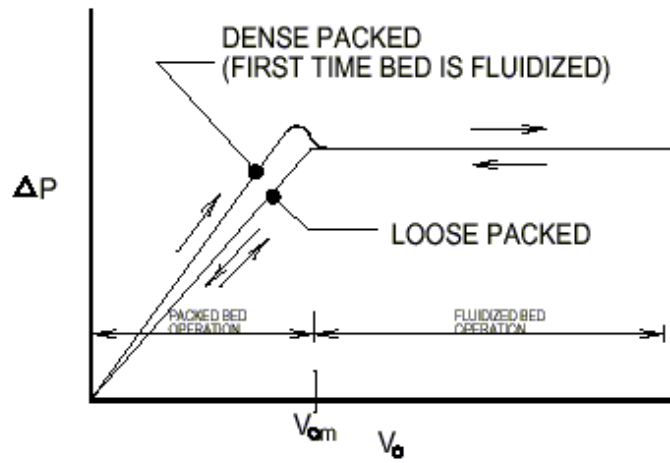
(3)

Ergun

$$\frac{1.75}{\mathbf{e}_f^3 \Phi} R_{ep_f}^2 + \frac{150(1 - \mathbf{e}_f)}{\mathbf{e}_f^3 \Phi^2} R_{ep_f} = N_{GA} \quad (6)$$

$$R_{ep_f} = \frac{\mathbf{r}V_{0f}d_p}{\mathbf{m}} \quad (7)$$

$$N_{GA} = \frac{d_p^3 \mathbf{r}(\mathbf{r}_p - \mathbf{r})g}{\mathbf{m}^2} \quad (8)$$



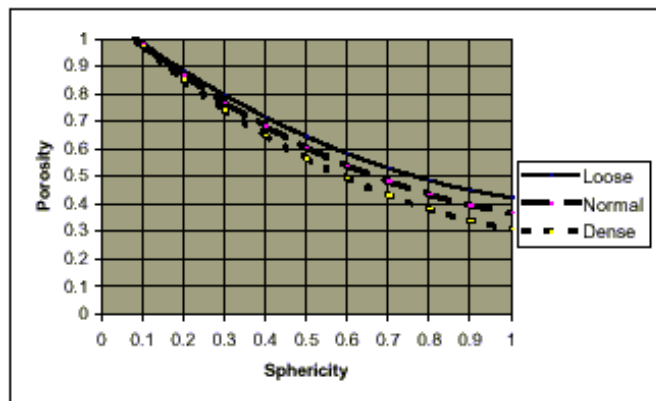
[3 : 對]

가 $R_{ep_f} < 1$, $R_{ep_f}^2$ Blake - Kozeny

$$\frac{150(1 - e_f)}{e_f^3 \Phi^2} R_{ep_f} = N_{GA} \dots \dots \dots \text{for } R_{ep_f} < 1 \quad (9)$$

$$V_{0f} = \frac{d_p^2 (r_p - r) g e_f^3 \Phi^2}{150 m (1 - e_f)} \quad (10)$$

[4 :]



가 가 .

e_{mf} Φ [4] 가 e_{mf}

V_{omf} Ergun

e_{mf} Φ 가 Ergun , (6)

$$K_2 R_{ep_{mf}}^2 + K_1 R_{ep_{mf}} = N_{GA} \quad (11)$$

$$K_1 = \frac{150(1 - e_{mf})}{e_{mf}^3 \Phi^2}, \quad K_2 = \frac{1.75}{e_{mf}^3 \Phi}$$

“ “ “ “ $0.001 < R_{ep_{mf}} < 4,000$ K_1

K_2 34% 가 V_{omf}

(11) K_1 K_2

$$R_{ep_{mf}} = \sqrt{\left(\frac{K_1}{2K_2}\right) + \frac{1}{K_2} N_{GA}} - \left(\frac{K_1}{2K_2}\right) \quad (12)$$

$$\left(\frac{K_1}{2K_2}\right) = 33.7, \quad \left(\frac{1}{K_2}\right) = 0.0408$$

K_1 K_2 [1]

[1 : (12)]

	$(K_1/2K_2)$	$1/K_2$	
	33.7	0.0408	Wen & Yu, AIChE J, 12(3) 610~612, 1966
	28.7	0.0494	Chitester etc. Chem.Eng.Sci., 39, 253, 1984

6.

가
가

V_{om_f}

가

V_{om_f}

()

가

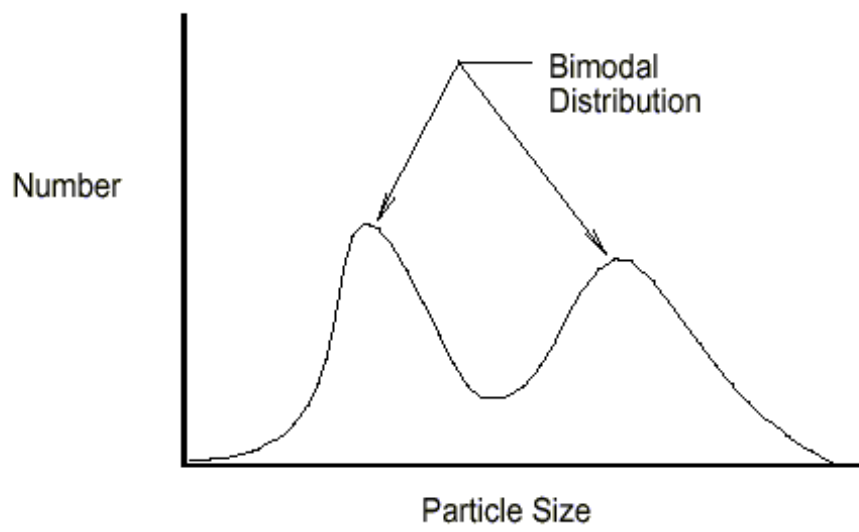
가

V_{om_f}

V_{om_f}

V_{om_f} 가

가

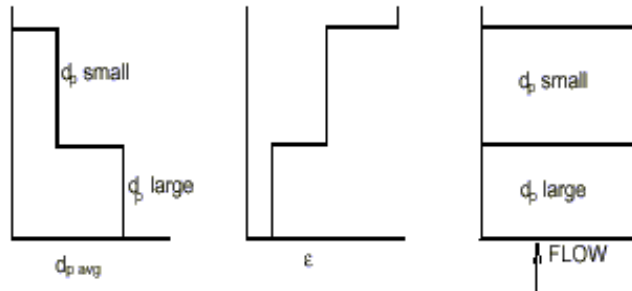


[5 : 2 () 2]

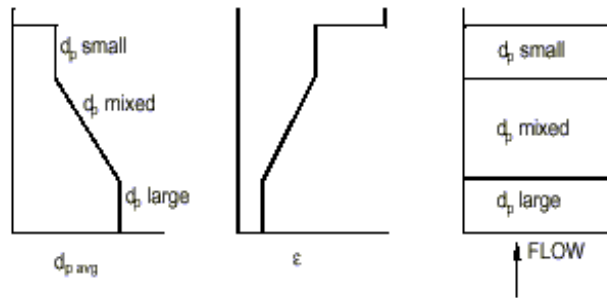
2 가 [5] 2 가 .

가
[6] .

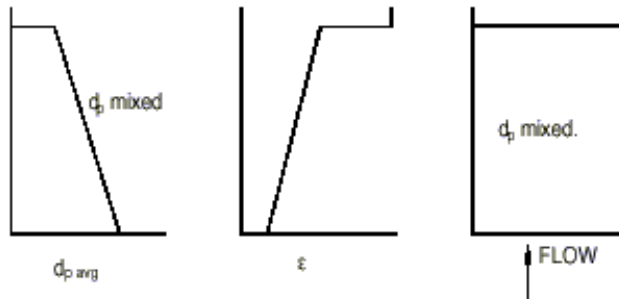
[6 : 2]



(a) 가 가 가 .



(b) 가
2 .



(c) 가 .